



## **Failure Modes, Effects and Diagnostic Analysis**

Project:

Surge protective devices LINETRAB LIT

Customer:

PHOENIX CONTACT GmbH & Co. KG  
Blomberg  
Germany

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## Management summary

This report summarizes the results of the hardware assessment carried out on the surge protective devices LINETRAB LIT in the versions listed in the drawings referenced in section 2.5.1. Table 1 gives an overview of the different configurations that belong to the considered surge protective devices LINETRAB LIT.

The hardware assessment consists of a Failure Modes, Effects and Diagnostics Analysis (FMEDA). A FMEDA is one of the steps taken to achieve functional safety assessment of a device per IEC 61508. From the FMEDA, failure rates are determined and consequently the Safe Failure Fraction (SFF) is calculated for the device. For full assessment purposes all requirements of IEC 61508 must be considered.

For safety applications only the described configurations were considered. All other possible variants or electronics are not covered by this report.

Surge protective devices are not considered to be elements according to IEC 61508-4 section 3.4.5 as they are not performing one or more element safety functions. Therefore, there is no need to calculate a SFF (Safe Failure Fraction). Only the interference on a safety functions needs to be considered. This interference is expressed in a contribution to the overall  $PFD_{AVG}$  / PFH.

The failure rates used in this analysis are from the *exida* Electrical Component Reliability Handbook ([N2]) for Profile 1 <sup>1</sup>.

**Table 1: Configuration overview LINETRAB LIT**

LIT 2-12	Surge protection in one-piece 6.2 mm wide DIN rail module for two floating signal wires; max. continuous operating voltage $U_c$ : 13 VAC / 18 VDC
LIT 4-12	Surge protection in one-piece 6.2 mm wide DIN rail module for four floating signal wires; max. continuous operating voltage $U_c$ : 13 VAC / 18 VDC
LIT 2-24	Surge protection in one-piece 6.2 mm wide DIN rail module for two floating signal wires; max. continuous operating voltage $U_c$ : 25 VAC / 36 VDC
LIT 4-24	Surge protection in one-piece 6.2 mm wide DIN rail module for four floating signal wires; max. continuous operating voltage $U_c$ : 25 VAC / 36 VDC
LIT 2x1-24	Surge protection in one-piece 6.2 mm wide DIN rail module for two conductors with common reference potential; max. continuous operating voltage $U_c$ : 25 VAC / 36 VDC
LIT 4x1-24	Surge protection in one-piece 6.2 mm wide DIN rail module for four conductors with common reference potential; max. continuous operating voltage $U_c$ : 25 VAC / 36 VDC
LIT 1x2-24	Surge protection in one-piece 6.2 mm wide DIN rail module for one floating signal circuit in 2-wire technology; max. continuous operating voltage $U_c$ : 25 VAC / 36 VDC
LIT 2x2-24	Surge protection in one-piece 6.2 mm wide DIN rail module for two floating signal circuits in 2-wire technology; max. continuous operating voltage $U_c$ : 25 VAC / 36 VDC

The following table shows how the above stated requirements are fulfilled under worst-case assumptions.

<sup>1</sup> See Appendix 3 for further details on the selected profile.

**Table 2: Summary for LIT 2-12 and LIT 2-24 – Failure rates <sup>2</sup>**

	<i>exida</i> Profile 1	
	Analysis 1 <sup>3</sup>	Analysis 2 <sup>4</sup>
<b>Failure category</b>	<b>Failure rates (in FIT)</b>	<b>Failure rates (in FIT)</b>
<b>Fail Safe Detected (<math>\lambda_{SD}</math>)</b>	<b>0</b>	<b>0</b>
<b>Fail Safe Undetected (<math>\lambda_{SU}</math>)</b>	<b>1.6</b>	<b>1.6</b>
<b>Fail Dangerous Detected (<math>\lambda_{DD}</math>)</b>	<b>0</b>	<b>1.4</b>
<b>Fail Dangerous Undetected (<math>\lambda_{DU}</math>)</b>	<b>7.8</b>	<b>6.4</b>
No effect	18	18
No part	0	0
<b>Total failure rate (interfering with safety function)</b>	<b>9.4 FIT</b>	<b>9.4 FIT</b>
<b>MTBF</b>	<b>3805 years</b>	<b>3805 years</b>

<sup>2</sup> It is assumed that complete practical fault insertion tests can demonstrate the correctness of the failure effects assumed during the FMEDA.

<sup>3</sup> Analysis 1 represents a worst-case analysis.

<sup>4</sup> Analysis 2 represents an analysis with the assumption that line short circuits and short circuits to GND are detectable or do not have an effect.

**Table 3: Summary for LIT 4-12 and LIT 4-24 – Failure rates <sup>5</sup>**

	<i>exida</i> Profile 1	
	Analysis 1 <sup>6</sup>	Analysis 2 <sup>7</sup>
<b>Failure category</b>	<b>Failure rates (in FIT)</b>	<b>Failure rates (in FIT)</b>
<b>Fail Safe Detected (<math>\lambda_{SD}</math>)</b>	<b>0</b>	<b>0</b>
<b>Fail Safe Undetected (<math>\lambda_{SU}</math>)</b>	<b>3.2</b>	<b>3.2</b>
<b>Fail Dangerous Detected (<math>\lambda_{DD}</math>)</b>	<b>0</b>	<b>2.8</b>
<b>Fail Dangerous Undetected (<math>\lambda_{DU}</math>)</b>	<b>15.6</b>	<b>12.8</b>
No effect	37	37
No part	0	0
<b>Total failure rate (interfering with safety function)</b>	<b>18.8 FIT</b>	<b>18.8 FIT</b>
<b>MTBF</b>	<b>1968 years</b>	<b>1968 years</b>

<sup>5</sup> It is assumed that complete practical fault insertion tests can demonstrate the correctness of the failure effects assumed during the FMEDA.

<sup>6</sup> Analysis 1 represents a worst-case analysis.

<sup>7</sup> Analysis 2 represents an analysis with the assumption that line short circuits and short circuits to GND are detectable or do not have an effect.

**Table 4: Summary for LIT 2x1-24 – Failure rates <sup>8</sup>**

	<i>exida</i> Profile 1	
	Analysis 1 <sup>9</sup>	Analysis 2 <sup>10</sup>
<b>Failure category</b>	<b>Failure rates (in FIT)</b>	<b>Failure rates (in FIT)</b>
<b>Fail Safe Detected (<math>\lambda_{SD}</math>)</b>	<b>0</b>	<b>0</b>
<b>Fail Safe Undetected (<math>\lambda_{SU}</math>)</b>	<b>2.7</b>	<b>2.7</b>
<b>Fail Dangerous Detected (<math>\lambda_{DD}</math>)</b>	<b>0</b>	<b>1.4</b>
<b>Fail Dangerous Undetected (<math>\lambda_{DU}</math>)</b>	<b>8.5</b>	<b>7.1</b>
No effect	18	18
No part	0	0
<b>Total failure rate (interfering with safety function)</b>	<b>11.2 FIT</b>	<b>11.2 FIT</b>
<b>MTBF</b>	<b>3768 years</b>	<b>3768 years</b>

<sup>8</sup> It is assumed that complete practical fault insertion tests can demonstrate the correctness of the failure effects assumed during the FMEDA.

<sup>9</sup> Analysis 1 represents a worst-case analysis.

<sup>10</sup> Analysis 2 represents an analysis with the assumption that line short circuits and short circuits to GND are detectable or do not have an effect.

**Table 5: Summary for LIT 4x1-24 – Failure rates <sup>11</sup>**

	<i>exida</i> Profile 1	
	Analysis 1 <sup>12</sup>	Analysis 2 <sup>13</sup>
<b>Failure category</b>	<b>Failure rates (in FIT)</b>	<b>Failure rates (in FIT)</b>
<b>Fail Safe Detected (<math>\lambda_{SD}</math>)</b>	<b>0</b>	<b>0</b>
<b>Fail Safe Undetected (<math>\lambda_{SU}</math>)</b>	<b>5.4</b>	<b>5.4</b>
<b>Fail Dangerous Detected (<math>\lambda_{DD}</math>)</b>	<b>0</b>	<b>2.8</b>
<b>Fail Dangerous Undetected (<math>\lambda_{DU}</math>)</b>	<b>17</b>	<b>14.2</b>
No effect	37	37
No part	0	0
<b>Total failure rate (interfering with safety function)</b>	<b>22.4 FIT</b>	<b>22.4 FIT</b>
<b>MTBF</b>	<b>1899 years</b>	<b>1899 years</b>

<sup>11</sup> It is assumed that complete practical fault insertion tests can demonstrate the correctness of the failure effects assumed during the FMEDA.

<sup>12</sup> Analysis 1 represents a worst-case analysis.

<sup>13</sup> Analysis 2 represents an analysis with the assumption that line short circuits and short circuits to GND are detectable or do not have an effect.

**Table 6: Summary for LIT 1x2-24 and LIT 2x2-24 – Failure rates <sup>14</sup>**

	<i>exida</i> Profile 1	
	Analysis 1 <sup>15</sup>	Analysis 2 <sup>16</sup>
<b>Failure category</b>	<b>Failure rates (in FIT)</b>	<b>Failure rates (in FIT)</b>
<b>Fail Safe Detected (<math>\lambda_{SD}</math>)</b>	<b>0</b>	<b>0</b>
<b>Fail Safe Undetected (<math>\lambda_{SU}</math>)</b>	<b>2.7</b>	<b>2.7</b>
<b>Fail Dangerous Detected (<math>\lambda_{DD}</math>)</b>	<b>0</b>	<b>3.9</b>
<b>Fail Dangerous Undetected (<math>\lambda_{DU}</math>)</b>	<b>5.8</b>	<b>1.9</b>
No effect	18	18
No part	0	0
<b>Total failure rate (interfering with safety function)</b>	<b>8.5 FIT</b>	<b>8.5 FIT</b>
<b>MTBF</b>	<b>4182 years</b>	<b>4182 years</b>

The failure rates are valid for the useful life of the surge protective devices LINETRAB LIT (see Appendix 2).

<sup>14</sup> It is assumed that complete practical fault insertion tests can demonstrate the correctness of the failure effects assumed during the FMEDA.

<sup>15</sup> Analysis 1 represents a worst-case analysis.

<sup>16</sup> Analysis 2 represents an analysis with the assumption that line short circuits and short circuits to GND are detectable or do not have an effect.

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## 1 Purpose and Scope

This document shall describe the results of hardware assessment according to IEC 61508 carried out on the surge protective devices LINETRAB LIT in the versions listed in the drawings referenced in section 2.5.1. Table 1 gives an overview of the different configurations that belong to the considered surge protective devices LINETRAB LIT.

The FMEDA builds the basis for an evaluation whether a sensor or final element subsystem, including the surge protective devices LINETRAB LIT meets the average Probability of Failure on Demand ( $PFD_{AVG}$ ) / Probability of dangerous Failure per Hour (PFH) requirements and if applicable the architectural constraints / minimum hardware fault tolerance requirements per IEC 61508 / IEC 61511. It **does not** consider any calculations necessary for proving intrinsic safety or the correct functioning of the surge protective devices.

## 2 Project management

### 2.1 *exida*

*exida* is one of the world's leading accredited Certification Bodies and knowledge companies specializing in automation system safety and availability with over 300 years of cumulative experience in functional safety. Founded by several of the world's top reliability and safety experts from assessment organizations and manufacturers, *exida* is a global company with offices around the world. *exida* offers training, coaching, project oriented system consulting services, safety lifecycle engineering tools, detailed product assurance, cyber-security and functional safety certification, and a collection of on-line safety and reliability resources. *exida* maintains a comprehensive failure rate and failure mode database on process equipment.

### 2.2 Roles of the parties involved

PHOENIX CONTACT GmbH & Co. KG Manufacturer of the surge protective devices  
LINETRAB LIT.

*exida* Performed the hardware assessment.

PHOENIX CONTACT GmbH & Co. KG contracted *exida* in January 2016 with the update of this report.

### 2.3 Standards / Literature used

The services delivered by *exida* were performed based on the following standards / literature.

[N1]	IEC 61508-2:2010	Functional Safety of Electrical/Electronic/Programmable Electronic Safety-Related Systems
[N2]	Electrical Component Reliability Handbook, 3rd Edition, 2012	<i>exida</i> LLC, Electrical Component Reliability Handbook, Third Edition, 2012, ISBN 978-1-934977-04-0

### 2.4 *exida* tools used

[T1]	SILcal V8.0.13	FMEDA Tool
[T2]	exSILentia V3.3.0.309	SIL Verification Tool

## 2.5 Reference documents

### 2.5.1 Documentation provided by the customer

[D1]	SIL- FMEDA-Bericht LIT ges..pdf	Overview of the devices with circuit diagrams and parts lists; Rev. 00 of 23.02.09
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The list above only means that the referenced documents were provided as basis for the FMEDA but it does not mean that *exida* checked the correctness and completeness of these documents.

### 2.5.2 Documentation generated by *exida*

[R1]	FMEDA_V7_LIT_2-12_V1R1.efm of 22.05.09
[R2]	FMEDA_V7_LIT_4-12_V1R1.efm of 22.05.09
[R3]	FMEDA_V7_LIT_2-24_V1R1.efm of 22.05.09
[R4]	FMEDA_V7_LIT_4-24_V1R1.efm of 22.05.09
[R5]	FMEDA_V7_LIT_2x1-24_V1R1.efm of 22.05.09
[R6]	FMEDA_V7_LIT_4x1-24_V1R1.efm of 22.05.09
[R7]	FMEDA_V7_LIT_1x2-24_V1R1.efm of 22.05.09
[R8]	FMEDA_V7_LIT_2x2-24_V1R1.efm of 22.05.09
[R9]	FMEDA_V7_LIT_1x2-24_2x2-24_w_ED_V1R1.efm of 11.03.2015
[R10]	FMEDA_V7_LIT_2-12_2-24_w_ED_V1R1.efm of 11.03.2015
[R11]	FMEDA_V7_LIT_2x1-24_w_ED_V1R1.efm of 11.03.2015
[R12]	FMEDA_V7_LIT_4-12_4-24_w_ED_V1R1.efm of 11.03.2015
[R13]	FMEDA_V7_LIT_4x1-24_w_ED_V1R1.efm of 11.03.2015

### 3 Description of the analyzed subsystems

The FMEDA of the surge protective devices LINETRAB LIT has been carried out on the parts indicated in Figure 1 to Figure 6.

The surge protective devices LIT 2-\* and LIT 4-\* are protective circuits for two or four floating signal wires. The maximum continuous operating voltage  $U_C$  is 13 VAC / 18 VDC for the -12 variants and 25 VAC / 36 VDC for the -24 variants.

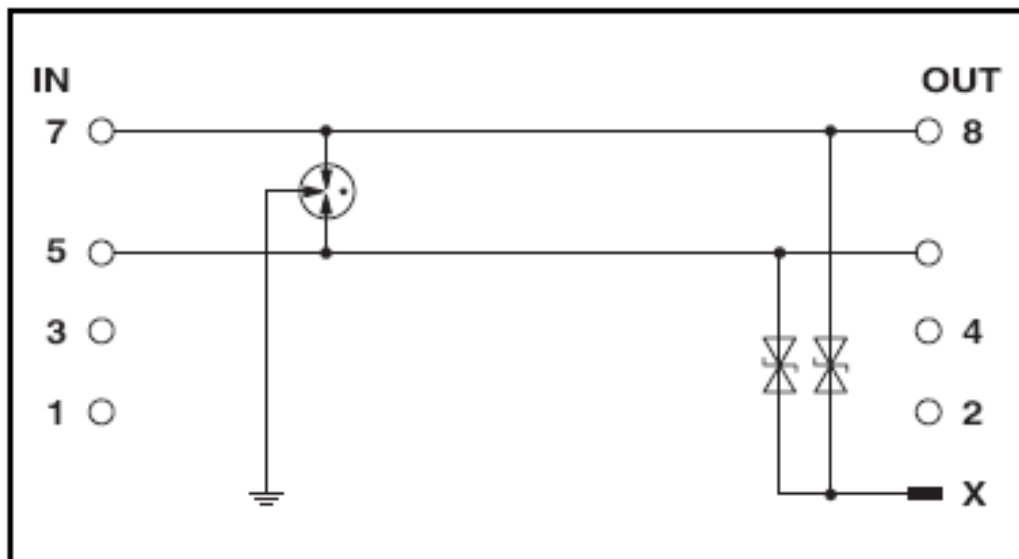


Figure 1: Block diagram of the surge protective device LIT 2-\*

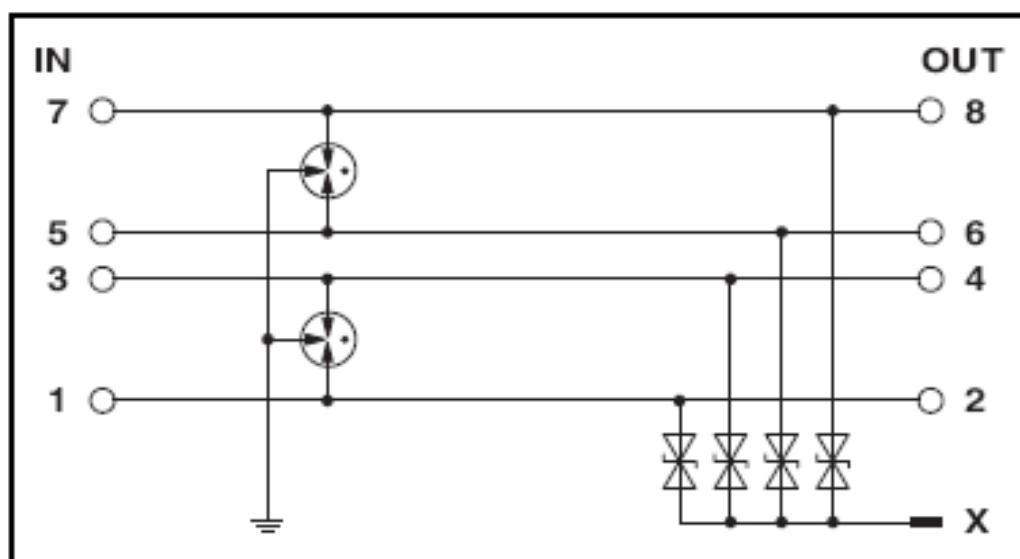


Figure 2: Block diagram of the surge protective device LIT 4-\*

The surge protective device LIT 2x1-24 offers surge protection in one-piece 6.2 mm wide DIN rail module for two conductors with common reference potential. The maximum continuous operating voltage  $U_c$  is 25 VAC / 36 VDC.

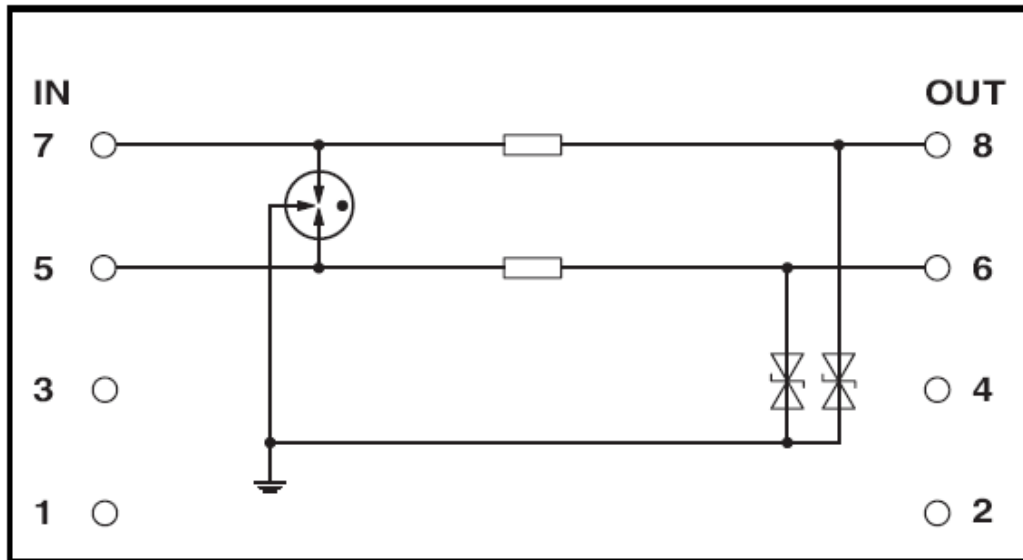


Figure 3: Block diagram of the surge protective device LIT 2x1-24

The surge protective device LIT 4x1-24 offers surge protection in one-piece 6.2 mm wide DIN rail module for four conductors with common reference potential. The maximum continuous operating voltage  $U_c$  is 25 VAC / 36 VDC.

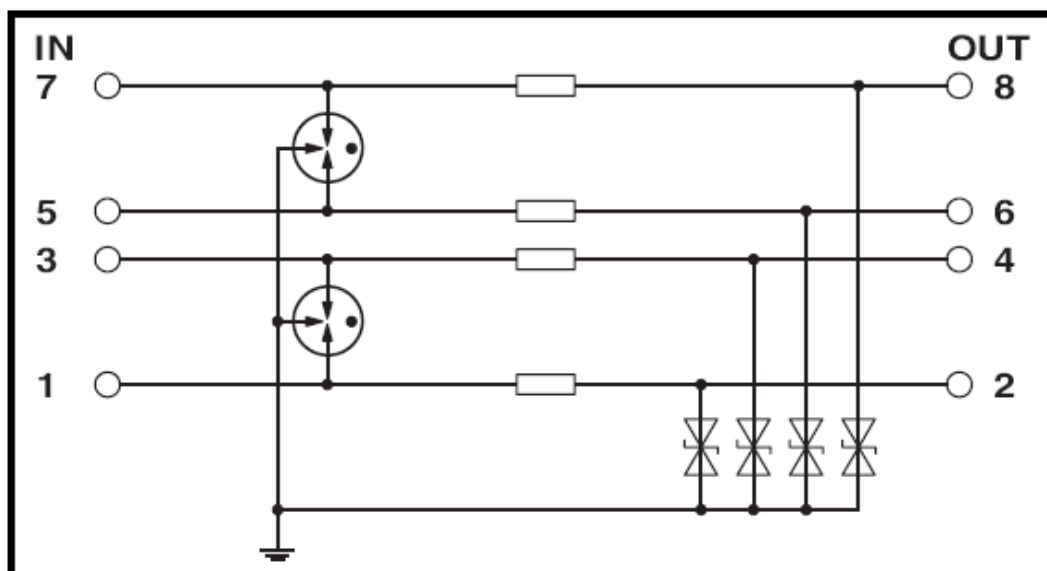


Figure 4: Block diagram of the surge protective device LIT 4x1-24

The surge protective device LIT 1x2-24 offers surge protection in one-piece 6.2 mm wide DIN rail module for one floating signal circuit in 2-wire technology. The maximum continuous operating voltage  $U_c$  is 25 VAC / 36 VDC.

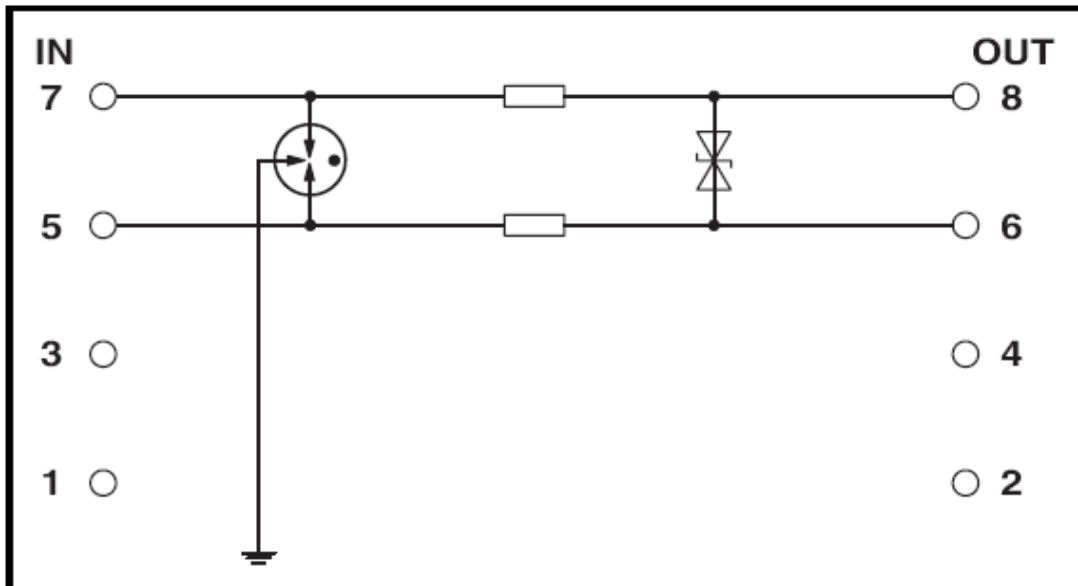


Figure 5: Block diagram of the surge protective device LIT 1x2-24

The surge protective device LIT 2x2-24 offers surge protection in one-piece 6.2 mm wide DIN rail module for two floating signal circuits in 2-wire technology. The maximum continuous operating voltage  $U_c$  is 25 VAC / 36 VDC.

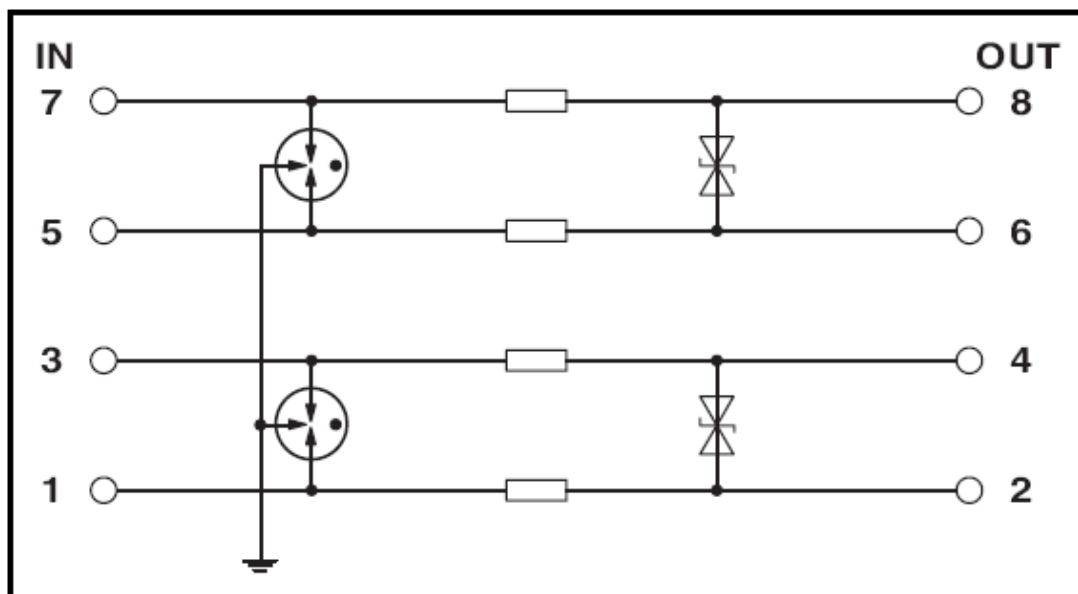
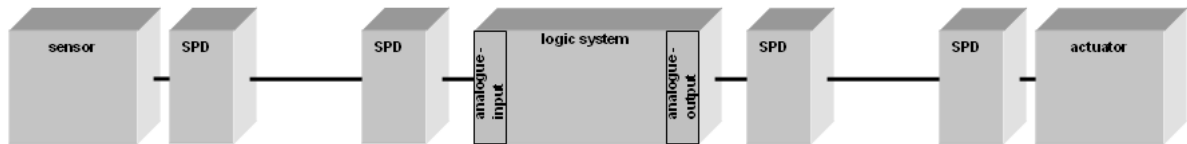
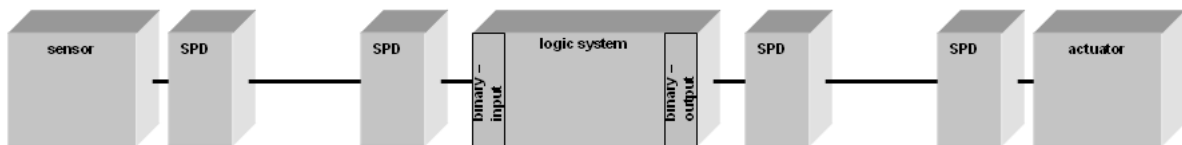


Figure 6: Block diagram of the surge protective device LIT 2x2-24

The following two figures Figure 7 and Figure 8 show how the surge protective devices can be connected to other devices. All considered surge protective devices can be used with analog or binary devices.



**Figure 7: Connection with analog devices**



**Figure 8: Connection with binary devices**

## 4 Failure Modes, Effects, and Diagnostic Analysis

The Failure Modes, Effects, and Diagnostic Analysis was done together with PHOENIX CONTACT GmbH & Co. KG and is documented in [R1] to [R13]. Failures have been classified according to the following failure categories.

### 4.1 Description of the failure categories

In order to judge the failure behavior of the surge protective devices LINETRAB LIT, the following definitions for the failure of the product were considered.

Fail-Safe State	The fail-safe state is defined as the output being de-energized or reaching the user defined threshold value or the predefined alarm state.
Safe	A safe failure (S) is defined as a failure that plays a part in implementing the safety function that: a) results in the spurious operation of the safety function to put the EUC (or part thereof) into a safe state or maintain a safe state; or, b) increases the probability of the spurious operation of the safety function to put the EUC (or part thereof) into a safe state or maintain a safe state.
Dangerous	A dangerous failure (D) is defined as a failure that plays a part in implementing the safety function that: a) prevents a safety function from operating when required (demand mode) or causes a safety function to fail (continuous mode) such that the EUC is put into a hazardous or potentially hazardous state; or, b) decreases the probability that the safety function operates correctly when required.
Dangerous Undetected	Failure that is dangerous and that is not being diagnosed by internal or external diagnostics (DU).
Dangerous Detected	Failure that is dangerous but is detected by external diagnostics (DD).
No effect	Failure mode of a component that plays a part in implementing the safety function but is neither a safe failure nor a dangerous failure.
No part	Component that plays no part in implementing the safety function but is part of the circuit diagram and is listed for completeness.



## 4.2 Methodology – FMEDA, Failure rates

### 4.2.1 FMEDA

A Failure Modes and Effects Analysis (FMEA) is a systematic way to identify and evaluate the effects of different component failure modes, to determine what could eliminate or reduce the chance of failure, and to document the system in consideration.

A FMEDA (Failure Modes, Effects, and Diagnostic Analysis) is a FMEA extension. It combines standard FMEA techniques with extension to identify online diagnostics techniques and the failure modes relevant to safety instrumented system design. It is a technique recommended to generate failure rates for each important category (safe detected, safe undetected, dangerous detected, dangerous undetected, fail high, fail low) in the safety models. The format for the FMEDA is an extension of the standard FMEA format from MIL STD 1629A, Failure Modes and Effects Analysis.

### 4.2.2 Failure rates

The failure rate data used by *exida* in this FMEDA is from the Electrical Component Reliability Handbook ([N2]) which was derived using over ten billion unit operational hours of field failure data from multiple sources and failure data from various databases. The rates were chosen in a way that is appropriate for safety integrity level verification calculations. The rates were chosen to match operating stress conditions typical of an industrial field environment similar to *exida* Profile 1. It is expected that the actual number of field failures due to random events will be less than the number predicted by these failure rates.

For hardware assessment according to IEC 61508 only random equipment failures are of interest. It is assumed that the equipment has been properly selected for the application and is adequately commissioned such that early life failures (infant mortality) may be excluded from the analysis.

Failures caused by external events however should be considered as random failures. Examples of such failures are loss of power or physical abuse.

The assumption is also made that the equipment is maintained per the requirements of IEC 61508 or IEC 61511 and therefore a preventative maintenance program is in place to replace equipment before the end of its “useful life”.

The user of these numbers is responsible for determining their applicability to any particular environment. Accurate plant specific data may be used for this purpose. If a user has data collected from a good proof test reporting system such as *exida* SILStat™ that indicates higher failure rates, the higher numbers shall be used. Some industrial plant sites have high levels of stress. Under those conditions the failure rate data is adjusted to a higher value to account for the specific conditions of the plant.

### 4.3 Assumptions

The following assumptions have been made during the Failure Modes, Effects, and Diagnostic Analysis of the surge protective devices LINETRAB LIT.

- Failure rates are constant, wear out mechanisms are not included.
- Propagation of failures is not relevant.
- The device is installed per manufacturer's instructions.
- The device is used within its specified limits.
- Sufficient tests are performed prior to shipment to verify the absence of vendor and/or manufacturing defects that prevent proper operation of specified functionality to product specifications or cause operation different from the design analyzed.
- For safety applications only the described configurations are considered.
- In case of multiple channel devices only one channel is part of the considered safety function.
- External power supply failure rates are not included.
- The mean time to restoration (MTTR) after a safe failure is 24 hours.

### 4.4 Results

For the calculation of the Safe Failure Fraction (SFF) the following has to be noted:

$\lambda_{\text{total}}$  consists of the sum of all component failure rates. This means:

$$\lambda_{\text{total}} = \lambda_{\text{SD}} + \lambda_{\text{SU}} + \lambda_{\text{DD}} + \lambda_{\text{DU}}$$

$$\text{MTBF} = \text{MTTF} + \text{MTTR} = (1 / (\lambda_{\text{total}} + \lambda_{\text{no effect}} + \lambda_{\text{no part}})) + 24 \text{ h}$$

#### 4.4.1 LIT 2-12 and LIT 2-24

The FMEDA carried out on the surge protective devices LIT 2-12 and LIT 2-24 leads under the assumptions described in sections 4.3 and 4.4 and the definitions given in section 4.1 to the following failure rates:

	<i>exida</i> Profile 1	
	Analysis 1 <sup>17</sup>	Analysis 2 <sup>18</sup>
<b>Failure category</b>	<b>Failure rates (in FIT)</b>	<b>Failure rates (in FIT)</b>
<b>Fail Safe Detected (<math>\lambda_{SD}</math>)</b>	<b>0</b>	<b>0</b>
<b>Fail Safe Undetected (<math>\lambda_{SU}</math>)</b>	<b>1.6</b>	<b>1.6</b>
<b>Fail Dangerous Detected (<math>\lambda_{DD}</math>)</b>	<b>0</b>	<b>1.4</b>
<b>Fail Dangerous Undetected (<math>\lambda_{DU}</math>)</b>	<b>7.8</b>	<b>6.4</b>
No effect	18	18
No part	0	0
<b>Total failure rate (interfering with safety function)</b>	<b>9.4 FIT</b>	<b>9.4 FIT</b>
<b>MTBF</b>	<b>3805 years</b>	<b>3805 years</b>

<sup>17</sup> Analysis 1 represents a worst-case analysis.

<sup>18</sup> Analysis 2 represents an analysis with the assumption that line short circuits and short circuits to GND are detectable or do not have an effect.

#### 4.4.2 LIT 4-12 and LIT 4-24

The FMEDA carried out on the surge protective devices LIT 4-12 and LIT 4-24 leads under the assumptions described in sections 4.3 and 4.4 and the definitions given in section 4.1 to the following failure rates:

	<i>exida</i> Profile 1	
	Analysis 1 <sup>19</sup>	Analysis 2 <sup>20</sup>
<b>Failure category</b>	<b>Failure rates (in FIT)</b>	<b>Failure rates (in FIT)</b>
<b>Fail Safe Detected (<math>\lambda_{SD}</math>)</b>	<b>0</b>	<b>0</b>
<b>Fail Safe Undetected (<math>\lambda_{SU}</math>)</b>	<b>3.2</b>	<b>3.2</b>
<b>Fail Dangerous Detected (<math>\lambda_{DD}</math>)</b>	<b>0</b>	<b>2.8</b>
<b>Fail Dangerous Undetected (<math>\lambda_{DU}</math>)</b>	<b>15.6</b>	<b>12.8</b>
No effect	37	37
No part	0	0
<b>Total failure rate (interfering with safety function)</b>	<b>18.8 FIT</b>	<b>18.8 FIT</b>
<b>MTBF</b>	<b>1968 years</b>	<b>1968 years</b>

<sup>19</sup> Analysis 1 represents a worst-case analysis.

<sup>20</sup> Analysis 2 represents an analysis with the assumption that line short circuits and short circuits to GND are detectable or do not have an effect.

#### 4.4.3 LIT 2x1-24

The FMEDA carried out on the surge protective device LIT 2x1-24 leads under the assumptions described in sections 4.3 and 4.4 and the definitions given in section 4.1 to the following failure rates:

	<i>exida</i> Profile 1	
	Analysis 1 <sup>21</sup>	Analysis 2 <sup>22</sup>
<b>Failure category</b>	<b>Failure rates (in FIT)</b>	<b>Failure rates (in FIT)</b>
<b>Fail Safe Detected (<math>\lambda_{SD}</math>)</b>	<b>0</b>	<b>0</b>
<b>Fail Safe Undetected (<math>\lambda_{SU}</math>)</b>	<b>2.7</b>	<b>2.7</b>
<b>Fail Dangerous Detected (<math>\lambda_{DD}</math>)</b>	<b>0</b>	<b>1.4</b>
<b>Fail Dangerous Undetected (<math>\lambda_{DU}</math>)</b>	<b>8.5</b>	<b>7.1</b>
No effect	18	18
No part	0	0
<b>Total failure rate (interfering with safety function)</b>	<b>11.2 FIT</b>	<b>11.2 FIT</b>
<b>MTBF</b>	<b>3768 years</b>	<b>3768 years</b>

<sup>21</sup> Analysis 1 represents a worst-case analysis.

<sup>22</sup> Analysis 2 represents an analysis with the assumption that line short circuits and short circuits to GND are detectable or do not have an effect.

#### 4.4.4 LIT 4x1-24

The FMEDA carried out on the surge protective device LIT 4x1-24 leads under the assumptions described in sections 4.3 and 4.4 and the definitions given in section 4.1 to the following failure rates:

	<i>exida</i> Profile 1	
	Analysis 1 <sup>23</sup>	Analysis 2 <sup>24</sup>
<b>Failure category</b>	<b>Failure rates (in FIT)</b>	<b>Failure rates (in FIT)</b>
<b>Fail Safe Detected (<math>\lambda_{SD}</math>)</b>	<b>0</b>	<b>0</b>
<b>Fail Safe Undetected (<math>\lambda_{SU}</math>)</b>	<b>5.4</b>	<b>5.4</b>
<b>Fail Dangerous Detected (<math>\lambda_{DD}</math>)</b>	<b>0</b>	<b>2.8</b>
<b>Fail Dangerous Undetected (<math>\lambda_{DU}</math>)</b>	<b>17</b>	<b>14.2</b>
No effect	37	37
No part	0	0
<b>Total failure rate (interfering with safety function)</b>	<b>22.4 FIT</b>	<b>22.4 FIT</b>
<b>MTBF</b>	<b>1899 years</b>	<b>1899 years</b>

<sup>23</sup> Analysis 1 represents a worst-case analysis.

<sup>24</sup> Analysis 2 represents an analysis with the assumption that line short circuits and short circuits to GND are detectable or do not have an effect.

#### 4.4.5 LIT 1x2-24 and LIT 2x2-24

The FMEDA carried out on the surge protective devices LIT 1x2-24 and LIT 2x2-24 leads under the assumptions described in sections 4.3 and 4.4 and the definitions given in section 4.1 to the following failure rates:

	<i>exida</i> Profile 1	
	Analysis 1 <sup>25</sup>	Analysis 2 <sup>26</sup>
<b>Failure category</b>	<b>Failure rates (in FIT)</b>	<b>Failure rates (in FIT)</b>
<b>Fail Safe Detected (<math>\lambda_{SD}</math>)</b>	<b>0</b>	<b>0</b>
<b>Fail Safe Undetected (<math>\lambda_{SU}</math>)</b>	<b>2.7</b>	<b>2.7</b>
<b>Fail Dangerous Detected (<math>\lambda_{DD}</math>)</b>	<b>0</b>	<b>3.9</b>
<b>Fail Dangerous Undetected (<math>\lambda_{DU}</math>)</b>	<b>5.8</b>	<b>1.9</b>
No effect	18	18
No part	0	0
<b>Total failure rate (interfering with safety function)</b>	<b>8.5 FIT</b>	<b>8.5 FIT</b>
<b>MTBF</b>	<b>4182 years</b>	<b>4182 years</b>

<sup>25</sup> Analysis 1 represents a worst-case analysis.

<sup>26</sup> Analysis 2 represents an analysis with the assumption that line short circuits and short circuits to GND are detectable or do not have an effect.

## 5 Using the FMEDA results

It is the responsibility of the Safety Instrumented Function designer to do calculations for the entire SIF. *exida* recommends the accurate Markov based exSILentia tool for this purpose. The following section describes how to apply the results of the FMEDA.

### 5.1 Example PFD<sub>AVG</sub> / PFH calculation for LIT 4x1-24

The following results must be considered in combination with PFD<sub>AVG</sub> / PFH values of other devices of a Safety Instrumented Function (SIF) in order to determine suitability for a specific Safety Integrity Level (SIL).

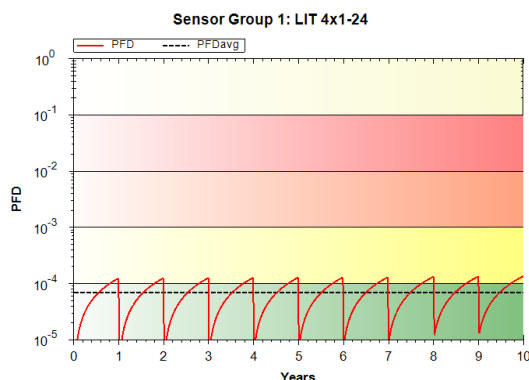
An average Probability of Failure on Demand (PFD<sub>AVG</sub>) calculation is performed for a single (1oo1) surge protective device LIT 4x1-24 (representing the worst-case of all considered devices) with *exida's* exSILentia tool. The failure rate data used in this calculation are displayed in section 4.4.4 for analysis 2. A mission time of 10 years has been assumed, a Mean Time To Restoration of 24 hours and a maintenance capability of 100%. Table 7 lists the results for different proof test intervals considering a proof test coverage of 99%(see Appendix 1.2).

**Table 7: PFD<sub>AVG</sub> / PFH values**

T[Proof] = 1 year	T[Proof] = 5 years	PFH
PFD <sub>AVG</sub> = 6.80E-05	PFD <sub>AVG</sub> = 3.16E-04	PFH = 1.43E-08 1/h

For SIL 2 the overall PFD<sub>AVG</sub> shall be better than 1.00E-02 and the PFH shall be better than 1.00E-06 1/h. As the surge protective devices are contributing to the entire safety function they should only consume a certain percentage of the allowed range. Assuming 5% of this range as a reasonable budget they should be better than or equal to 5.00E-04 or 5.00E-08 1/h, respectively. The PFH value and the calculated PFD<sub>AVG</sub> value for a proof test interval of 1 year are within the allowed range for SIL 2 according to table 2 of IEC 61508-1 and do fulfill the assumption to not claim more than 5% of the allowed range, i.e. to be better than or equal to 5.00E-04 or 5.00E-08 1/h, respectively.

The resulting PFD<sub>AVG</sub> graph generated from the exSILentia tool for a proof test of 1 year is displayed in Figure 9.



**Figure 9: PFD<sub>AVG</sub>(t)**

An average Probability of Failure on Demand (PFD<sub>AVG</sub>) calculation performed for redundant (1oo2) surge protective devices (according to analysis 2) considering a proof test coverage of 99% (see Appendix 1.1), a mission time of 10 years, a Mean Time To Restoration of 24 hours, a maintenance capability of 100% and a common cause factor of 10% would result in a PFD<sub>AVG</sub> value of 6.80E-06 for a one year proof test interval.



## 6 Terms and Definitions

FIT	Failure In Time ( $1 \times 10^{-9}$ failures per hour)
FMEDA	Failure Modes, Effects, and Diagnostic Analysis
HFT	Hardware Fault Tolerance
Low demand mode	Mode where the frequency of demands for operation made on a safety-related system is no greater than one per year and no greater than twice the proof test frequency.
High demand mode	Mode, where the frequency of demands for operation made on a safety-related system is greater than twice the proof check frequency.
MTBF	Mean Time Between Failure
$PFD_{AVG}$	Average Probability of Failure on Demand
PFH	Probability of dangerous Failure per Hour
SFF	Safe Failure Fraction summarizes the fraction of failures which lead to a safe state and the fraction of failures which will be detected by diagnostic measures and lead to a defined safety action.
SIF	Safety Instrumented Function
SIL	Safety Integrity Level
SPD	Surge Protective Device
T[Proof]	Proof Test Interval

## 7 Status of the document

### 7.1 Liability

*exida* prepares reports based on methods advocated in International standards. Failure rates are obtained from a collection of industrial databases. *exida* accepts no liability whatsoever for the use of these numbers or for the correctness of the standards on which the general calculation methods are based.

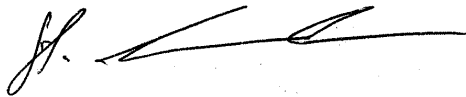
Due to future potential changes in the standards, best available information and best practices, the current FMEDA results presented in this report may not be fully consistent with results that would be presented for the identical product at some future time. As a leader in the functional safety market place, *exida* is actively involved in evolving best practices prior to official release of updated standards so that our reports effectively anticipate any known changes. In addition, most changes are anticipated to be incremental in nature and results reported within the previous three year period should be sufficient for current usage without significant question.

Most products also tend to undergo incremental changes over time. If an *exida* FMEDA has not been updated within the last three years and the exact results are critical to the SIL verification you may wish to contact the product vendor to verify the current validity of the results.

### 7.2 Releases

Version History: V2R0: Report layout updated and second analysis added;  
March 14, 2016  
V1R0: Review comments incorporated; June 12, 2009  
V0R1: Initial version; May 28, 2009  
Author: Stephan Aschenbrenner  
Review: V0R1: Steffen Pförtner (PHOENIX CONTACT); June 8, 2009  
Rachel Amkreutz (*exida*); June 8, 2009  
Release status: Released to PHOENIX CONTACT GmbH & Co. KG

### 7.3 Release Signatures



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Dipl.-Ing. (Univ.) Stephan Aschenbrenner, Partner



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Rachel Amkreutz, Safety Engineer

## Appendix 1: Possibilities to reveal dangerous undetected faults during the proof test

According to section 7.4.5.2 f) of IEC 61508-2 proof tests shall be undertaken to reveal dangerous faults which are undetected by diagnostic tests.

This means that it is necessary to specify how dangerous undetected faults which have been noted during the FMEDA can be detected during proof testing.

Appendix 1 shall be considered when writing the safety manual as it contains important safety related information.

### Appendix 1.1: Proof test to detect dangerous undetected faults

A suggested proof test consists of the following steps, as described in Table 8.

**Table 8 Steps for a possible proof Test**

Step	Action
1	Bypass the connected safety device(s) or take other appropriate action to avoid a false trip
2	Force the surge protective devices LINETRAB LIT to reach predefined output signals over the entire range and verify that the output behaves as expected.
3	Restore the loop to full operation
4	Remove the bypass from the connected safety device(s) or otherwise restore normal operation

This test will detect approximately 99% of possible “du” failures of the surge protective devices LINETRAB LIT.

## Appendix 2: Impact of lifetime of critical components on the failure rate

According to section 7.4.7.4 of IEC 61508-2, a useful lifetime, based on experience, should be assumed.

Although a constant failure rate is assumed by the probabilistic estimation method (see section 4.3) this only applies provided that the useful lifetime<sup>27</sup> of components is not exceeded. Beyond their useful lifetime the result of the probabilistic calculation method is therefore meaningless, as the probability of failure significantly increases with time. The useful lifetime is highly dependent on the component itself and its operating conditions – temperature in particular (for example, electrolytic capacitors can be very sensitive).

This assumption of a constant failure rate is based on the bathtub curve, which shows the typical behavior for electronic components. Therefore, it is obvious that the  $PFD_{AVG}$  calculation is only valid for components which have this constant domain and that the validity of the calculation is limited to the useful lifetime of each component.

It is assumed that early failures are detected to a huge percentage during the installation period and therefore the assumption of a constant failure rate during the useful lifetime is valid.

The surge protective devices LINETRAB LIT do not contain components with reduced useful lifetime which are contributing to the dangerous undetected failure rate and therefore to the  $PFD_{AVG}$  calculation. Therefore, there is no limiting factor to the useful lifetime.

When plant experience indicates a shorter useful lifetime than indicated in this appendix, the number based on plant experience should be used.

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<sup>27</sup> Useful lifetime is a reliability engineering term that describes the operational time interval where the failure rate of a device is relatively constant. It is not a term which covers product obsolescence, warranty, or other commercial issues.

### Appendix 3: *exida* Environmental Profiles

<i>exida</i> Profile	1	2	3	4	5	6
<b>Description (Electrical)</b>	Cabinet mounted/ Climate Controlled	Low Power Field Mounted  no self-heating	General Field Mounted  self-heating	Subsea	Offshore	N/A
<b>Description (Mechanical)</b>	Cabinet mounted/ Climate Controlled	General Field Mounted	General Field Mounted	Subsea	Offshore	Process Wetted
<b>IEC 60654-1 Profile</b>	B2	C3 also applicable for D1	C3 also applicable for D1	N/A	C3 also applicable for D1	N/A
<b>Average Ambient Temperature</b>	30C	25C	25C	5C	25C	25C
<b>Average Internal Temperature</b>	60C	30C	45C	5C	45C	Process Fluid Temp.
<b>Daily Temperature Excursion (pk-pk)</b>	5C	25C	25C	0C	25C	N/A
<b>Seasonal Temperature Excursion (winter average vs. summer average)</b>	5C	40C	40C	2C	40C	N/A
<b>Exposed to Elements/Weather Conditions</b>	No	Yes	Yes	Yes	Yes	Yes
<b>Humidity<sup>28</sup></b>	0-95% Non-Condensing	0-100% Condensing	0-100% Condensing	0-100% Condensing	0-100% Condensing	N/A
<b>Shock<sup>29</sup></b>	10 g	15 g	15 g	15 g	15 g	N/A
<b>Vibration<sup>30</sup></b>	2 g	3 g	3 g	3 g	3 g	N/A
<b>Chemical Corrosion<sup>31</sup></b>	G2	G3	G3	G3	G3	Compatible Material
<b>Surge<sup>32</sup></b>						
Line-Line	0.5 kV	0.5 kV	0.5 kV	0.5 kV	0.5 kV	N/A
Line-Ground	1 kV	1 kV	1 kV	1 kV	1 kV	
<b>EMI Susceptibility<sup>33</sup></b>						
80MHz to 1.4 GHz	10V /m	10V /m	10V /m	10V /m	10V /m	N/A
1.4 GHz to 2.0 GHz	3V/m	3V/m	3V/m	3V/m	3V/m	
2.0GHz to 2.7 GHz	1V/m	1V/m	1V/m	1V/m	1V/m	
<b>ESD (Air)<sup>34</sup></b>	6kV	6kV	6kV	6kV	6kV	N/A

<sup>28</sup> Humidity rating per IEC 60068-2-3

<sup>29</sup> Shock rating per IEC 60068-2-27

<sup>30</sup> Vibration rating per IEC 60068-2-6

<sup>31</sup> Chemical Corrosion rating per ISA 71.04

<sup>32</sup> Surge rating per IEC 61000-4-5

<sup>33</sup> EMI Susceptibility rating per IEC 6100-4-3

<sup>34</sup> ESD (Air) rating per IEC 61000-4-2